

REF: NEGMASS1.MCD

# Dynamic Field Mass Analysis

by  
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Previous mass field analysis concerned a static end point analysis of the field mass of a transmission line. It was shown that the negative mass at a quarter wavelength was best illustrated if we could take a snapshot in time. Unfortunately, the cyclic nature of a standing wave field will tend to cause the field mass to swing through both positive as well as negative values wherein the sum of the excursions will tend to balance out to zero field mass. This analysis looks at the end of the line as being dynamic and will look at a possible method of isolating the desired field mass excursion in time so as to provide for gravitational control referenced to the local gravitational field of a near mass such as the Earth. First, the constants related to the analysis are presented below. All are in SI units.

$$\mu_0 := 1.256637061 \cdot 10^{-06}$$

Magnetic permeability.

$$m_e := 9.109389700 \cdot 10^{-31}$$

Electron rest mass.

$$q_e := 1.602177330 \cdot 10^{-19}$$

Electron charge.

$$c := 2.997924580 \cdot 10^{08}$$

Speed of light in a vacuum.

$$h := 6.626075500 \cdot 10^{-34}$$

Plank constant.

$$r_q := 2.817940920 \cdot 10^{-15}$$

Classical electron radius.

Let:  $i_{line} := 1 \cdot 10^{06}$  amp

and  $f_{line} := 1 \cdot 10^{08}$  Hz

Then:

$$d_{line} := \frac{c}{f_{line}}$$

or,

$$d_{line} = 2.99792458 \text{ meter}$$

Again, my previous field mass analysis' assumed a fixed phase at the end of a transmission line. Therefore the result was the instantaneous value which is not representative of what is occurring over a full cycle. The below formulae show how this occurs if the phase angle is assumed to be constant.

Let:

$$\theta := \frac{\pi}{2}$$

and

$$i_{SW} := i_{line} \cdot e^{j \cdot \theta}$$

then:

$$i_{SW} = 6.123031769111886 \cdot 10^{-11} + 1 \cdot 10^8 i \quad \text{amp}$$

Then the effective mass related to purely reactive current wave is given below as:

$$m_{SW} := \left( \mu_0 \cdot \frac{i_{SW}^2}{4 \cdot \pi \cdot l \cdot q} \right) \cdot \left( \frac{d_{line}}{c} \right)^2 \quad \text{eq. 1}$$

or,

$$m_{SW} = -3.548690437601892 \cdot 10^3 + 4.34574885763599 \cdot 10^{-13} i \quad \text{kg}$$

**For example: If various values of phase angle between 0 and 2 pi is input in the above equation, a full range of field mass from positive to negative and real to imaginary will result in the output of eq. 1.**

**The idea of a horizontal rotation of the end of a transmission line located at the perimeter of a UFO style craft seems to me to be a close approximation for what is observed concerning the field mechanics of flying saucers. Using PIN diodes to switch (open or short) the end of the transmission line at the appropriate times to achieve negative or positive mass may be possible. When the end of the line at the perimeter is shorted or open, the beginning of the line at the center of the saucer is open or shorted respectively. It may be possible to pump up the signal on the line to very large values with a PIN diode switching method. There may be placed parallel to the transmission line a field storage line or permeable 'skin' that will return field energy to the main line during the proper times related to the PIN diode switching event.**

**Let us define a changing parameter at the end of a line, which, when rotated through space horizontally, is equivalent to a changing wavelength along a virtual transmission line: (Previous analysis was for a point at the end of a non-moving line.)**

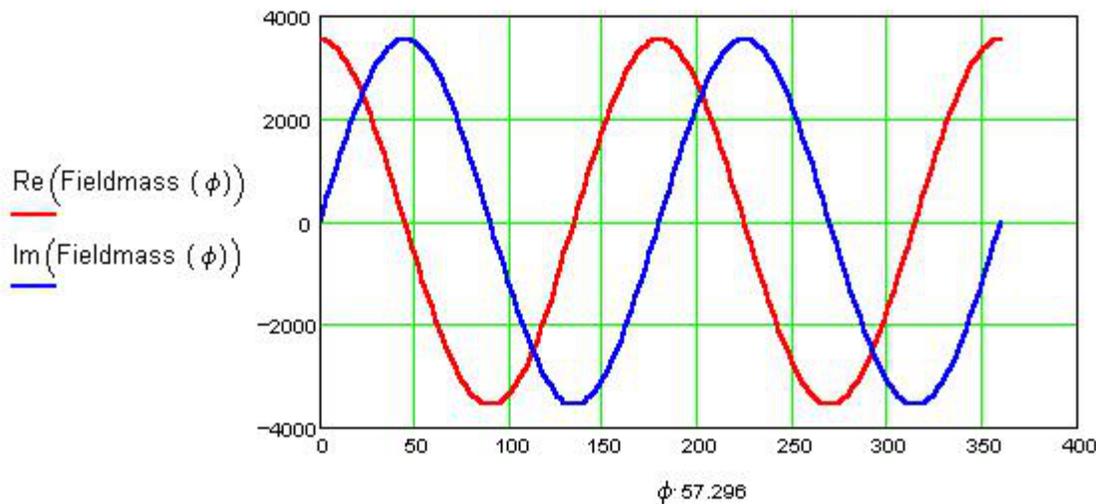
**Let:**

$$\phi := 0.00 \cdot \pi, 0.01 \cdot \pi \dots 2 \cdot \pi$$

$$i(\phi) := i_{line} \cdot e^{j \cdot \phi}$$

then:

$$\text{Fieldmass}(\phi) := \left( \mu_0 \cdot \frac{i(\phi)^2}{4 \cdot \pi \cdot l \cdot q} \right) \cdot \left( \frac{d_{line}}{c} \right)^2 \quad \text{eq. 2}$$



Plot 1

It is apparent in the above graph that the real component (mass) is shadowed by the imaginary component (mass) separated by 90 degrees lag from the real component (mass). Then we will also define herein that a change of length along the line, related to the fixed wavelength and frequency, is equivalent to a change in *phase* along the wave created by the motion that is generated by the virtual transmission line as described above.

Normally, a change of phase is meant to convey a change in time between two signals, where one is the reference signal and the other is the time displaced signal. The above plot represents a fixed frequency phase plot between real and imaginary field mass space. Then for all real space field mass there would exist an imaginary space field mass lagging real space field mass by 90 degrees.

The summation of all real or imaginary field mass points through 180 degrees along the transmission line shown above will yield by summation a net zero field mass. Previous papers on negative mass field generation stipulated quarter wave field generation which will yield a negative only field mass. However, if the result in the red line is summed over a length of the line within the beginning 90 degree portion of the line, the net result will balance out to zero in the real space field mass case. In this analysis, let us expect that It is the real space result which is of importance to real space action. Therefore, in order that we may generate a net positive or negative field mass, it is suggested by the above plot that 0 to 45 degrees or 45 to 90 degrees may be generated respectively.

Professor Stavros G. Dimitriouhas suggested that creating an unbalanced non-symmetrical waveform in the amplitude sense along the line will create a local acceleration. This has been explored very well by Professor Stavros both theoretically and experimentally. We have at least two possible ways to generate an unbalanced sum of points along the virtual line above. Firstly, by amplitude distortion or phase distortion, or even a combination of both. For example: We could force a non-linearity in the waveform amplitude by putting a diode across the input to the transmission line. This would cause the waveform to become lopsided in the amplitude which would cause a net negative or positive real field mass to be generated.

Unfortunately, the force output has been limited by the fact that a changing field tends to cycle and smooth out the force offset towards a net sum of near zero.

This next analysis might be called dynamic transfer analysis since it looks at the end of a transmission line end-on while the end is moving to the right horizontally. What is created is a 'virtual' transmission line since it is a vertical motion transposed to the right by linear displacement which creates a sine wave that can be analyzed as a transmission line action.

If we allow for a translation to the right of only a quarter wavelength then we end up with the below plot.

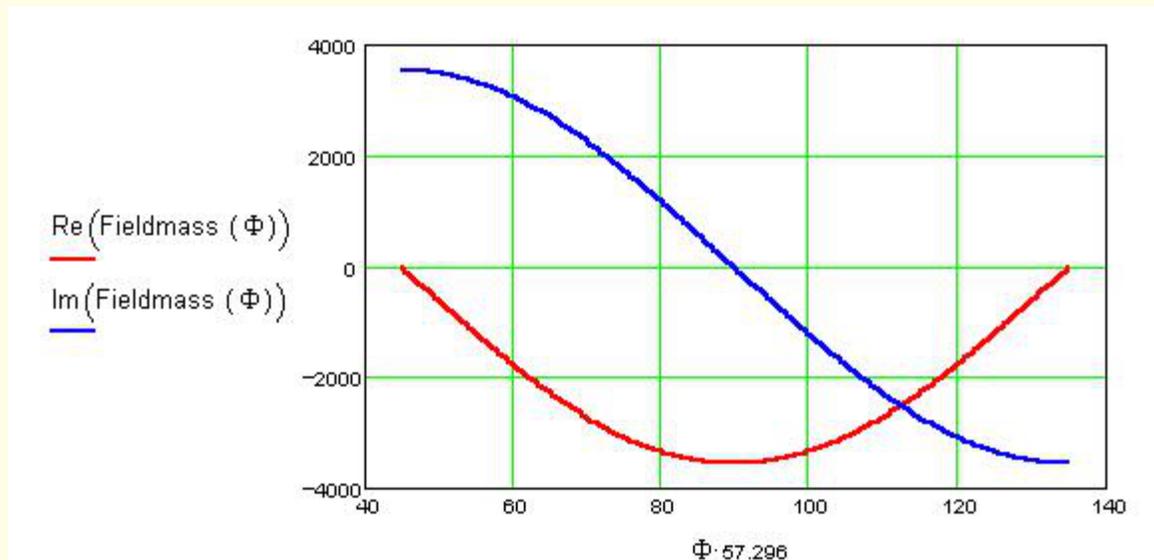
Let:

$$\Phi := 1.0 \cdot \frac{\pi}{4}, 1.01 \cdot \frac{\pi}{4} \dots \frac{3 \cdot \pi}{4}$$

$$i(\Phi) := i_{\text{line}} \cdot e^{j \cdot \Phi}$$

$$\text{Fieldmass}(\Phi) := \left( \mu_0 \cdot \frac{i(\Phi)^2}{4 \cdot \pi \cdot l \cdot q} \right) \cdot \left( \frac{d_{\text{line}}}{c} \right)^2$$

eq. 3



Plot 2

Plot 2 above is shown for a linear displacement to the right of the end of the main transmission line during the 1/4 to 3/4 wavelength portion at the end of the line. This suggests that timing or gating the linear displacement of the end of the line to coincide with the desired attraction or repulsion result from the above field mass equation will allow for either greater or diminished negative or positive field mass as required for control of the vehicle relative to a local gravitational field. This approach will allow for a 100% field mass offset.

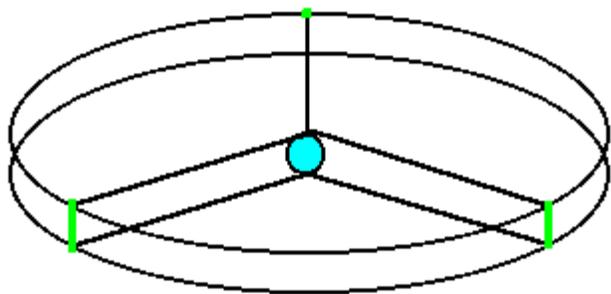
The timing of the horizontal displacement was adjusted to provide for the maximum negative mass in the above plot. The action described in creating the virtual transmission line is equivalent to a rotation (pivoting) of the transmission line around its input in the horizontal plane so as to maximize the negative or positive mass result for action in the vertical sense. Note that the imaginary field mass is now summed up to be equal to zero.

Again, a parallel line or permeable outer skin acting as a field storage secondary can be used to return the energy to the main transmission line at the appropriate times depending on the end point switch timing in the main transmission line.

UFO's, or flying saucers, have been observed to have what appears to be a rotating field around them. One account that I read about observed that there appeared to be waves of energy rolling down around a craft in a vertical motion like waves of honey around a honey dipper. This was observed while the craft was at a landing site. As the craft lifted, this rolling field was perhaps shifted into a horizontal mode similar to the virtual rotation of the end of the transmission line above to convert the stored field energy to negative mass.

Obviously, a huge amount of field energy is connected with electrogravitational and/or mass-field generation. This field may have to be built up over some period of time and would be characterized by a large amount of building field momentum. The parallel transmission line I proposed above is likely only one way that the field energy could be pumped up and stored for each succeeding cycle of field mass action.

Below is an animated picture of how I suspect the field around a UFO is generated.



### UFO Field mass generation

The above animation shows by vertical green bars the currents being switched into shorted vertical conductors at the perimeter of a UFO style craft by PIN diodes. The perimeter vertical green bars represent super conductive elements that can handle currents of a million amps or greater which is necessary to generate the required negative mass field. The PIN diodes are located near the beginning of the transmission line where the black lines that radiate outward begin. The magenta stripes represent the negative mass field that is generated at the perimeter of the craft during the 1/4 to 3/4 phase sequence as shown on plot 2 above. The red vertical lines represent the voltage at the top and bottom of the craft which are the same polarity with respect to each other.

The 3/4 to 5/4 phase is the portion that has no horizontal switching action. This is accompanied by a blue vertical line at the top and bottom of the craft which also represents building and decaying potential voltage. Then the maximum mass offset (or differential) is assured by properly timing the switching that creates the virtual transmission line around the perimeter of the craft. Having the top and bottom of the craft at the same relative voltage polarity ensures that the action will not radiate as with a conventional antenna action.

The above animation shows that the duration of the mass creation and the resting no mass creation are equal. The total being 180 degrees. This is equivalent to 1/2 spin for a fermion such as an electron. Since I am modeling the field mechanics of a UFO style craft to be quantum capable, this is to be expected. If we wished to plot the graph of positive mass, a phase range of  $-1/8$  to  $+1/8$  lambda, (-45 to + 45 degrees), would be necessary.

To allow for motion horizontally, we could adjust one of the three sections shown in the animation to fire every other time ( or every third time, etc.) and this would cause an offset force around the rim of the craft. This is by reason that since we are generating a rotating mass field around the perimeter, the force offset would be related to the familiar

$F = mv^2/r$  equation.

In summary, the concepts presented in this paper represent my latest work concerning quantum mechanical electrogravitational propulsion and control. I feel that this may be very close to the actual field mechanics of some UFO style craft. Finally, this is an ongoing work and therefore may be revised and updated as necessary.

---Jerry E. Bayles.

[Back to the MAIN PAGE.](#)